OBSERVATION OF CHARGE COMPENSATED POLARIZATION ZONES IN POLYVINYLINDENFLUORIDE (PVDF) FILMS BY PIEZOELECTRIC ACOUSTIC STEP-WAVE RESPONSE

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A high resolution $(2 \mu m)$ acoustic step-wave probing techniques has been developed to investigate the inhomogeneous distribution of the piezoelectric response of incompletely corona poled 85 μ m thick PVDF films We observe persistent polarization zones or layers of 20–40 μ m width within the films which are electrostatically compensated by charge accumulation at the polarization zone boundaries The zone development is explained by charge-trapping in proportion to polarization

POLYMERS with molecular chains carrying a transverse dipole moment as PVDF (polyvinylidenfluoride) are strongly piezoelectric and pyroelectric [1-11] after poling by corona discharge or by high electric fields Whereas most experiments concerning the basic nature of piezoelectricity and pyroelectricity in this system indicate the importance of dipole orientation in crystallites of the polymer (cf [2]), there is a lack of knowledge with respect to the detailed nature of the polarization process, especially since inhomogeneous polarization distributions [10, 11] by incomplete poling have been observed

In this communication we report the observation of charge compensated finite width polarization zones within film generated during incomplete poling This gives evidence for the coupling of charge-injection, -transport and -accumulation to dipole orientation in the poling process [12] of PVDF

For the experimental analysis of inhomogeneous charge, polarization or piezoelectric distributions in dielectric films, an acoustic pressure or velocity step (AVS) method, as first described by Laurenceau et al [16], has been applied We achieved resolution improvement of two orders of magnitude by generating the pressure or velocity step function, instead of using a shock tube [16], by the transient response of a piezoelectric crystal [17] (e.g. X-quartz) to a short risetime voltage pulse The PVDF-film is directly coupled to the generating crystal by a thin silicon oil film (d < 2000 Å) As depicted in Fig 1, rectangular electrical pulses are applied to the X-quartz crystal (diameter = 25 mm, thickness = 3 mm). With the detector electrode coupled to a B&H, Model AC 3011 low noise wide band preamplifier, the signal is either displayed on a Tektronix 7104 scope or x-y recorded, using a Philips PM 3400 sampling scope

By the piezoelectric transient response [17] of the

quartz disk, rectangular acoustic pulses propagate from both surfaces into the crystal and are transmitted into the PVDF sample The particle velocity in the transmitted wave for the pulse starting from the sound soft crystal backside according to acoustic transient response and boundary conditions is given by, cf [17],

$$v = \frac{2Z_1}{Z_1 + Z_2} k \sqrt{\left(\frac{\epsilon_0 \epsilon_1}{\rho_1}\right)} \frac{V}{d}$$
(1)

v is the step-wave particle velocity in the film, Z_1 and Z_2 are the acoustic longitudinal wave impedance in quartz and in the film, respectively, k, e_1 , ρ_1 and d are the piezoelectric coupling constant for longitudinal waves, high frequency dielectric constant, density and thickness of the X-quartz plate, respectively, e_0 is the vacuum dielectric constant and V is the pulse voltage amplitude

The calibration of the piezoelectric response according to equations (1) and (2), see below, by using a thin X-quartz crystal (d = 0.19 mm) instead of the PVDF film, cf Fig 1 (insert), reveals a rectangular response signal (risetime = 1 ns) within 5% of the calculated signal amplitude For a film sound velocity [18] of $(2.2 \pm 0.07) \times 10^5$ cm sec⁻¹, the overall risetime of 1 nsec corresponds to $2\,\mu$ m resolution of the electrical active film structures These can be layered distributions of polarization, space charge or intrinsic piezoelectricity which are revealed by single or multiple signal current maxima, cf Figs 2 and 3, during step wave propagation in the film The detailed analysis [19] of the corresponding total signal results in the following relation

$$I_{s}(t) = \frac{A}{l} v \left| (1+\gamma) \left\{ \sigma_{1} + \int_{0}^{x_{s}} \rho(x) dx \right\} - e(x_{s}) - \gamma P_{0}(x_{s}) \right|$$

$$(2)$$

with $I_s(t) =$ short circuit signal current, cf Fig 1,



Fig 1 Schematic representation of the experimental technique (1) Connection to voltage pulse generator, 400 V, 150 psec risetime, 100 nsec pulse duration, 100 Hz repetition rate (2) Connection to wide-band preamplifier and oscilloscope *Insert* current response signal $I_s(t)$ of a 0 19 thick x-quartz plate, effective electrode diameter 4 6 mm, pre-amplification factor = 10

 $x_s = v_s t$ step from position after propagation time t, A = sample area, l = sample thickness, v = velocity amplitude in the step-wave, $v_s =$ step propagation velocity, $\gamma = -(1/\xi)(\partial \epsilon/\partial s)$ relative electrostriction coefficient

$$\sigma_1 = \frac{1}{l} \int_0^l P_0(x) dx - \int_0^l \left(1 - \frac{x}{l}\right) \rho(x) dx$$

static counter charge per area on the grounding electrode of the sample under short circuit condition, $\rho(x)$ spacecharge density in the sample volume coupled to the particle velocity of the step wave, $e(x_s) =$ intrinsic piezoelectric constant, $P_0(x_s) =$ persistent polarization in the unstrained film Note Changes of oriented elementary dipole moments by strain (direct contribution to be considered small for PVDF [2]) or by local strain induced electrostriction [2] are contained in $e(x_s)$, whereas the elementary dipolemoments of $p_0(x)$ by definition do not change under strain In deriving equation (2), Maxwell's equation, and the strain s = $-v/v_s$ in the step wave have been used

Since in our experiments σ_1 in general turns out to be zero, we discuss the situation of complete field neutralization by the condition $\rho(x) = \partial P_0(x)/\partial x$, i.e. the space charge distribution is in electrostatic equilibrium with the persistent polarization. In this case equation (2), even with finit electrostriction γ , reduces to

$$I_{s}(t) = \frac{A}{l} v |P_{0}(x_{s}) - e(x_{s})|, \qquad (3)$$

where $P_0(x_s)$ can be replaced by $\int_0^{x_s} \rho(x) dx$, since $I_s(t)$ is due to the movement of charges and not to the movement of elementary dipoles with constant dipole moment



Fig 2 Acoustic step response signal $I_s(t)$ of a thermally poled 88 μ m thick PVDF film with high content of α -form crystallites, poling conditions Voltage 1 8 kV, time 1 hr, temperature 120°C, evaporated Al-electrodes Pre-amplification factor = 83, effective electrode diameter = 5 mm x_s = step position in the PVDF film The step wave enters the positive poled side of the film, $x_s = 0$, with positive particle velocity in propagation direction

Our measurements of $I_s(t)$ show the following results For a *thermally* poled film (thickness 88 μ m) we observe (Fig 2) a positive $I_s(t)$ signal at the pluspolarity-poling electrode with the sharp onset corresponding to the instrumental resolution of 2 μ m The signal decays to the zero baseline indicating the absence of polarization and space charges in the sample volume towards the negative poling electrode in agreement with the results of Phelan *et al* [10] and Sussner and Dransfeld [11] for *incomplete poling*

For films (thickness $85 \,\mu\text{m}$) incompletely poled at room temperature by a positive $18 \,\text{kV}$ corona point discharge, the $I_s(t)$ signals for different poling times are shown in Figs 3(a-d) These results reveal for the first time polarization zones or layers completely confined to the film interior without signal contributions at the film boundaries The single zones in Figs 3(a-c) show the same halfwidth of approx $30\,\mu\text{m}$ and increase in amplitude roughly linear with poling time until a maximum is reached after about 20 sec For longer poling times the amplitude of the single zone decreases to zero, followed by the development of double zone structures, as shown in Fig 3(d)

The absence of signal contributions, Figs 3(a-d), at the film boundaries indicates zero charge density $\sigma_1 = 0$ on the grounding electrode (as also $\sigma_2 = 0$, charge density on the detecting electrode) and consequently complete field neutralization [22] by compensating space charge accumulation at the polarization zone boundaries, as consistent with the finite electrical conductance in PVDF (dielectric relaxation time [1] 10^2 sec) From this follows that the signal current is described by equation (3) By corresponding



Fig 3 Acoustic step response signal $I_s(t)$ of plus corona point discharge poled PVDF films with high content of α -form crystallites for different poling times. Poling condition Voltage plus 18 kV, point electrode distance 1 3 cm, films in contact with grounded copper electrode, no evaporated electrodes, room temperature. Poling times (a) 7 sec, (b) 13 sec, (c) 17 sec, (d) 4 min The step wave enters the positive poled side of the film, $x_s = 0$, with positive particle volocity in propagation direction Pre-amplification factor = 83, effective electrode diameter = 5 mm. The $x_s = 0$ and $x_s = l$ positions were determined by delay time calibration

quantitative evaluation of our measurement we obtain maximum [21] persistent $P_0(x)$ values of $8 \,\mu\text{C}\,\text{cm}^{-2}$ comparable with literature data [2] and with the estimated value of $10\,\mu\text{C}\,\text{cm}^{-2}$, based on our poling conditions injection current density $1\,\mu\text{A}\,\text{cm}^{-2}$, poling time 20 sec, and persistent (zero field-remnant) polarization amounting to approx 50% of the total polarization at maximum field

From this follows that the roughly time-proportional polarization zone development, Figs 3(a-c), can be described as a charging process of an intrinsic capacitive layer with reduced conductance The decrease of conductance must be directly caused by polarization, since the unpolarized material appears to be homogeneous Corresponding to this model, we solved the non-linear differential equation of charge-injection, -transport and -polarization with charge trapping [15] in proportion to polarization, obtaining internal polarization [23] in agreement with our observations Polarization-proportional trapping, therefore, provides the necessary feedback mechanism causing internal field enhancement by reducing the effective charge mobility, 1 e the conductance decrease of an internal zone Our calculation shows that the width of the polarization free boundary zone increases with the logarithm of the ratio of charge mobility and injection current density, indicating also the conditions for homogeneous poling Microscopically, charge trapping in proportion to polarization may be due to trapping at oriented dipoles at the crystallite surface [23]

In explaining the transition from a single zone [Figs 3(a-c)] to a double zone [Fig 3(d)], we expect that after reaching the saturation polarization of the crystallites, a further field increase leads to charge detrapping by the Poole–Frenkel [24] effect With "soft" intrinsic ferroelectricity [25, 26] of the crystallites, charge detrapping causes the decay of polarization in the first zone [Fig 3(c)] by "discharge", which is consistent with our observations. The detrapped charges, together with the charges injected from the film surface, then initiate the development of the double zone structure [Fig 3(d)] by the same mechanisms, discussed with respect to the development of the first polarization zone. We believe that the strongly assymmetric polarization in Fig 2 can also be described [27] by our model

Since our observation of internal polarization zones is consistent with charge injection and polarizationproportional charge trapping, we believe that this mechanism is also responsible for the high electrical and thermal stability [25] of polarization in PVDF or other polar polymers

The AVS-technique appears also useful for investigations of polarization and charge distributions in real charge electrets [28] and possibly for charge distributions at metal-insulator or metal-semiconductor interfaces [29]

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