## Supplementary Material

## 1 SUPPLEMENTARY DATA



Figure S1: Setup of the cylindrical simulation geometry of length 1.47 m and diameter of 0.02 m . The pressure drop is calculated between the pressure sensors p1 and p2. The suspension flows from left to right.

Table S1. Simulation setup for different software packages.

| Abbreviation |  |  | AF-DD AF-BS | OF-BS | OF-FG | COM ${ }^{1}$ | SPH ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Solver |  |  | Pressure-based |  |  | direct linear solver <br> (PARADISO) | Single Phase FlowNN |
| Model |  |  | Viscous laminar | Laminar |  | Viscous laminar | BinghamPapanastasiou |
| Solution method | Pressure Velocity Coupling | scheme | SIMPLE |  |  | Fully coupled | - |
|  | Discretization | Gradient | Least Square Cell Based | Gaus | linear | - | - |
|  |  | Pressure | Second order | $\begin{aligned} & \text { Gauss } \\ & \text { (2.order } \end{aligned}$ | $\begin{aligned} & \text { Tinear } \\ & \text { central) } \end{aligned}$ | First/Second order | Tait EOS |
|  |  | Momentum | Second order Upwind | $\begin{aligned} & \text { Gauss } \\ & \text { (2.order } \end{aligned}$ | $\begin{aligned} & \text { Tinear } \\ & \text { central) } \end{aligned}$ | First/Second order | Tait EOS |
|  |  | Time ${ }^{3}$ |  |  |  | - | Velocity Verlet |

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Figure S2: Mesh of pipe cross-section created with Ansys ICEM CFD for coarsest (L0) and finest resolution (L3).


Figure S3: Initial fluid particle distribution for coarsest (R0) and finest resolution (R3) used in the SPH method.


Figure S4: Velocity profiles for different mesh refinements modeled with the software OpenFOAM (FG). The data is shown for the bi-viscous model in the $c v$ case. The lines connect the numerical points as guidance of the eye. The plug-flow region is also shown enlarged for $u=0.37-0.41 \mathrm{~m} \mathrm{~s}^{-1}$.


Figure S5: Velocity profile $u(r)$ for different regularization parameters $\nu_{0}$ in the OpenFOAM solution for the bi-viscous model ( $c v$ ). The analytical solution is drawn as continuous line, the numerical results at the center of the grid cells are shown as points. The dashed lines connect the numerical points as guidance of the eye. The plug-flow region is also shown enlarged for $u=0.39-0.41 \mathrm{~m} \mathrm{~s}^{-1}$.


Figure S6: Viscosity profile $\nu(r)$ for different regularization parameters $\nu_{0}$ in the OpenFOAM solution for the bi-viscous model (cv). The analytical solution is drawn as continuous lines, the numerical results at the center of the grid cells are shown as points. The dashed lines connect the numerical points as guidance of the eye.


Figure S7: Velocity profile $u(r)$ for different regularization parameters $m$ in the OpenFOAM solution for the Papanastasiou model (cv). The analytical solution is drawn as continuous lines, the numerical results at the center of the grid cells are shown as points. The dashed lines connect the numerical points as guidance of the eye. The plug-flow region is also shown enlarged for $u=0.395-0.408 \mathrm{~m} \mathrm{~s}^{-1}$.


Figure S8: Viscosity profile $\nu(r)$ for different regularization parameters $m$ in the OpenFOAM solution for the Papanastasiou model (cv). The analytical solution is drawn as continuous lines, the numerical results at the center of the grid cells are shown as points. The dashed lines connect the numerical points as guidance of the eye.


[^0]:    ${ }^{1}$ The basic Lagrange functions are 1st order for the Bingham model and 2nd order for Bingham-Papanastasiou model.
    ${ }^{2}$ Further information about SPH method is provided in section 2.2.5.4
    ${ }^{3}$ For the mesh-based methods, steady state simulations were used. Only SPH needs a transient time scheme.

