

A SPATIAL LIGHT MODULATOR USING BSO CRYSTALS

F HOLLER and H J TIZIANI

Institut für Technische Optik, Universität Stuttgart, Pfaffenwaldring 9, D-7000 Stuttgart 80, Fed Rep Germany

Received 24 October 1985, revised manuscript received 23 December 1985

The combined use of the photoelectric and electro-optic properties of the $\text{Bi}_{12}\text{SiO}_{20}$ (BSO)-crystal leads to a new possibility of realizing a spatial light modulator. Under certain geometrical conditions, which will be discussed, it is possible to realize, that the BSO-crystal becomes birefringent depending on the local illuminance, the physical connection between the distributions of birefringence and illuminance will be shown. The BSO-crystal combined with a polarizer setup works as a spatial light modulator or as an incoherent to coherent converter.

1. Introduction

To avoid speckling and other phase disturbances in coherent optical image processing it is recommendable to use a two dimensional incoherent to coherent (IC)-converter working in real time. A spatial light modulator (SLM) working in real time, which converts illuminance into transparency, works as such an IC-converter.

Most of the currently existing spatial light modulators work according to the following principle. A photoconductive material modulates an applied electric field (or alternating field) along the optical axes in dependence on the local (incoherent) illuminance. Another electrooptic material converts the modulation of the applied electric field into a modulation of birefringence. A suitable polarizer setup converts the modulation of birefringence into a modulation of transmission. The complete optical setup therefore works as an incoherent to coherent (IC)-converter.

Some SLM's use liquid crystals as the electrooptic material and CdS [1,2] or $\text{Bi}_{12}\text{SiO}_{20}$ (BSO) - crystals [3] as the photoconductive material, they are rather expensive and their response time is not satisfying. Other concepts working with two materials are the microchannel spatial light modulator (MSLM) [4] and the DKDP-converter [5,6]. The limit of spatial resolution of the MSLM and the response time of the DKDP-converter do not satisfy the need for most of the applications.

Several concepts of holographic IC-conversion have been realized up to now. The deformable surface spatial light modulator [7] is limited to 10 lines/mm spatial resolution and works with two materials.

Another principle of holographic IC-conversion [8] requires only one material, which is able to store a holographic grating in real time such as the BSO-crystal. The intensity of the incoherent illumination deforms the grating accordingly. The main disadvantage of the holographic IC-conversion is the necessity of a holographic optical setup in order to write the grating.

Our aim therefore was to find a material working as well photoconductively electrooptically. Bulk monocrystalline BSO is a suitable material [9-11]. If the optical axis and the applied electric field are mutually perpendicular, the crystal will become birefringent depending on the local illuminance [12,13].

2. Spatial light modulation in BSO-crystals

Physical mechanisms for light pattern recording and erasure in BSO are drift and trapping of photoelectrons under illumination by incoherent (or coherent) light in the transverse electrooptic configuration. This gives rise to a space charge field modulating the refractive index via the linear electrooptic effect [14]. Erasure can be achieved by uniform illumination of the crystal.

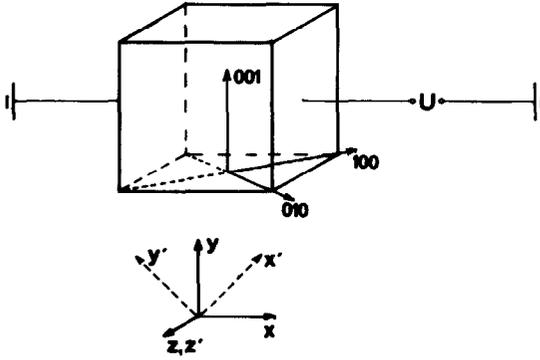


Fig. 1 Crystal orientation (100), (010), (001) crystal axes, z optical axis of image formation, x direction of the extant electric field, x' , y' , z' optical axes of the crystal

The modulation of the refractive index by the space charge field E_{sc} is described by the following equation

$$n = n_0 - 0.5 n_0^3 r_{41} E_{sc}$$

$$r_{41} = 5 \times 10^{-7} \text{ cm/kV (see ref [11])} \quad (1)$$

Fig. 1 shows the orientation of the crystal's major optical axes. Local birefringence resp polarization change is the result of two different physical effects [13]

(i) The linear electrooptic effect leads to an anisotropic spatial modulation of the refractive index, which is described by the following equations (see fig 1)

$$n_{x'} = n_0 - 0.5 \cos(45^\circ) n_0^3 r_{41} E_{sc}$$

$$n_{y'} = n_0 + 0.5 \cos(45^\circ) n_0^3 r_{41} E_{sc} \quad (2)$$

(ii) The electrogyratory effect, i.e. the dependence of optical activity with the space charge field.

The space charge field induced by the illumination needs to be calculated. In the case of a sinusoidal grating $I(x) = I_0(1 + m \cos kx)$ of high intensity ($I_0 > 1 \text{ mW/cm}^2$) and low modulation ($m \ll 1$) the steady state value of the space charge field in the drift dominant recording mode is given in ref [15]

$$E_{sc}(x) = E_0 m \cos kx \quad (3)$$

For the more general case $0 \leq m \leq 1$ the crystal response is no longer linear and the space charge field is given by the following formula (15)

$$E_{sc}(x) = E_0 (1 - m_1^2)^{1/2} / (1 + m_1 \cos kx)^{1/2} \quad (4)$$

m_1 is the reduced modulation given by formula (5) where n_D is the carrier concentration in the dark and τg_0 means the carrier concentration under incident illumination I_0

$$m_1 = m \tau g_0 / (\tau g_0 + n_D) \quad (5)$$

Combining eqs (2) and (4) leads to

$$n = \begin{pmatrix} n_{x'} \\ n_{y'} \end{pmatrix} = \begin{pmatrix} n_0 \\ n_0 \end{pmatrix} + \frac{r_{41} \cos 45^\circ}{2} n_0^3 \frac{(1 - m_1^2)^{1/2}}{1 + m_1 \cos kx} \times E_0 \begin{pmatrix} -1 \\ +1 \end{pmatrix} \quad (6)$$

This result shows, that the crystal's birefringence is modified depending on the local illumination. Combined with an appropriate polarizer setup the crystal works as a spatial light modulator or as an incoherent to coherent converter.

The physical mechanisms can be summarized as follows. The BSO-crystal, a cubic electrooptic crystal, becomes birefringent when a voltage is applied between the (110)-faces for instance. If the incident light is plane, polarized and orientated to bisect the birefringent axes, the light leaving the BSO-crystal will be elliptically polarized. If we project an incoherent image into the crystal, the light intensity distribution leads to the appropriate absorption, carriers are generated in the light struck areas. These photo-generated carriers move in the electric field in a direction to neutralize the applied field thereby reducing the electric field and hence the birefringence. This leads to the spatial light modulator with the appropriate polarizer arrangement.

When the crystal was placed between crossed polarizers combined with a quarter wave plate compensating the natural birefringence [13] of the crystal, it was possible to convert a modulation of birefringence into a modulation of transmission. Fig. 2 shows the optical setup used.

By changing the angle between polarizer and analyzer a positive or negative image can be selected. Figs 3 and 4 show this clearly. Fig 5 shows the spectrum of an incoherently illuminated grating after IC-conversion.

The spatial resolution is very often not only lim-

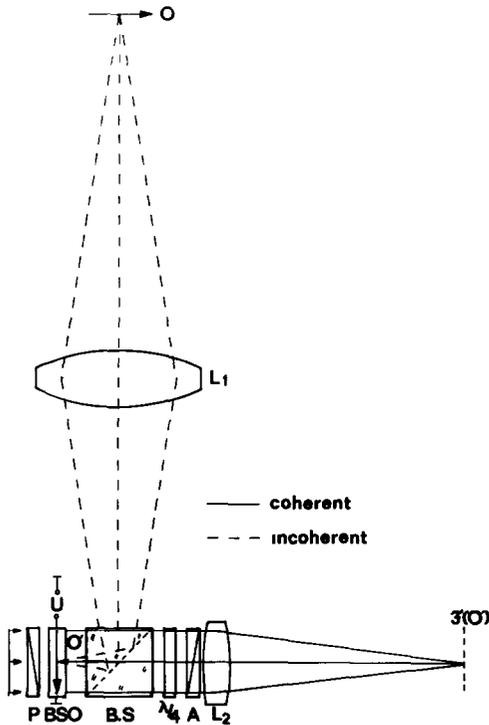


Fig 2 Optical setup used B S Beamsplitter, $\lambda/4$ quarter-waveplate, A analyzer, P polarizer, L_1 lens for incoherent image formation, L_2 Fourier transform lens.

ited by the crystal's properties but also by the crystal's geometry. Because of the thickness d of the crystal a slightly defocussed image occurs.

The light sensitivity of the crystal depends on the crystal's absorption, namely

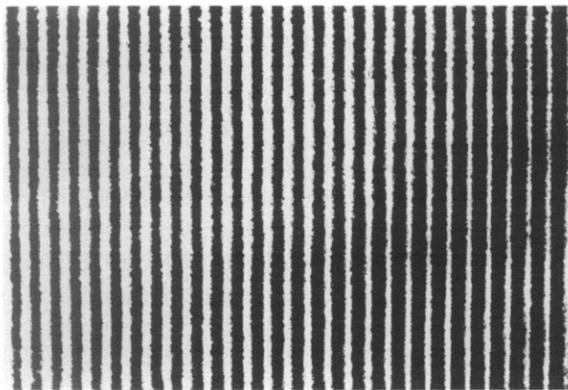


Fig 3. IC-converted picture of a lattice with a spatial frequency of 10 lines/mm

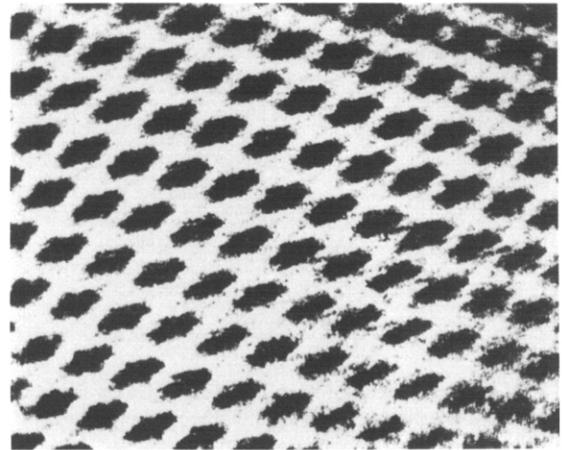


Fig. 4 IC-converted and contrast reversed picture of an electrical shaver's blade

$$S = \text{const} [1 - \exp(-\alpha d)] \tag{7}$$

Here α is the absorption coefficient of the crystal. Therefore a very thin crystal is not appropriate for our application.

The optical transfer function $D(R)$, on the other hand, depends on the aperture ratio, the lateral magnification β of the incoherent image formation and the thickness d of the crystal. The complete optical transfer function $D_c(R, z)$, where z represents the amount of defocussing, is given by

$$D_c(R, z) = D_{\text{BSO}}(R) D_{\text{opt}}(R) D_{\text{def}}(R, z) \tag{8}$$

where $D_{\text{BSO}}(R)$ resp $D_{\text{opt}}(R)$ are the OTF's of the BSO-crystal resp the optical system used. $D_{\text{def}}(R, z)$ represents the OTF due to defocussing.

When reading out the BSO with a plane wave with

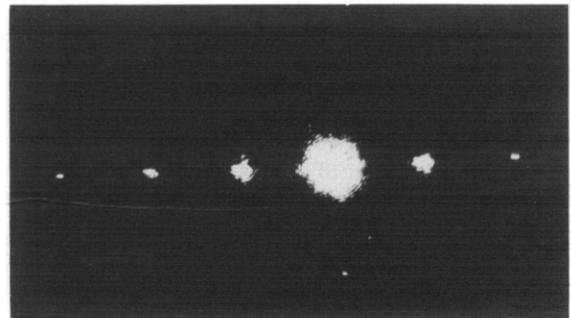


Fig 5 Fourier spectrum of the lattice shown in fig 3 after IC-conversion

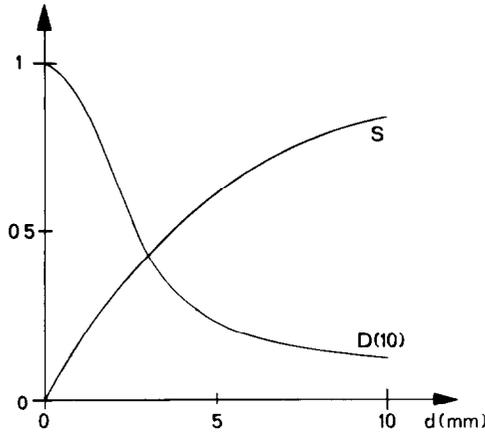


Fig. 6. Modulation transfer function $D(10$ lines/mm) (aperture ratio 1.4) and sensitivity S in dependence on the crystal's thickness d

the assumption of small absorption one will get

$$D(R) = D_{\text{BSO}}(R)D_{\text{opt}}(R) \frac{2}{d} \int_0^{d/2} D_{\text{def}}(R, z) dz \quad (9)$$

$D_{\text{def}}(R, z)$ is given by the following formula

$$D_{\text{def}}(R, z) = J_1(2\pi Rz \tan \sigma') / (2\pi Rz \tan \sigma') \quad (10)$$

σ' represents the aperture angle in the BSO-crystal. Combining formulas (9) and (10) gives

$$D(R) = D_{\text{BSO}}(R) D_{\text{opt}}(R) (2/d') \times [(d'/2)J_0(d'/2) + J_1(0) - J_1(d'/2) + (d'/2)J_1(d'/2)H_0(d'/2) - (d'/2)J_0(d'/2)H_1(d'/2)], \quad (11)$$

where $d' = d \cdot 2\pi R \tan \sigma'$

For practical applications a compromise between maximum optical transfer function and maximum sensitivity is needed. Fig. 6 shows a good compromise for d between 1 mm and 5 mm thickness. Our experiments were carried out with crystals of a thickness of 2.7 mm.

3. Experimental results

According to eq. (6) the electrooptic effect linearly depends on the applied electric field. The surrounding atmosphere limits the possible electric field

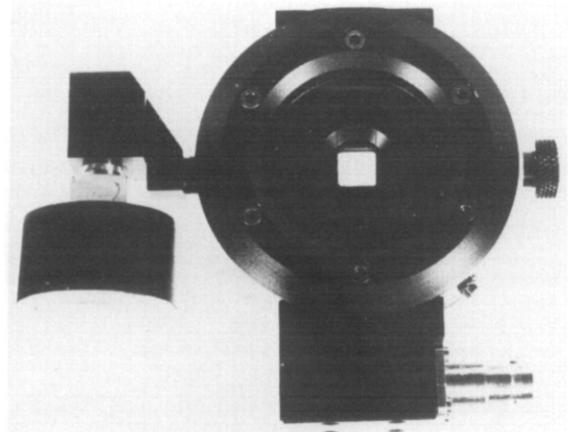


Fig. 7. Pressure chamber used. The chamber is able to endure 10 bar pressure and more than 10 kV/cm.

to about 5 kV/cm, otherwise electrical lightnings could damage the crystal.

Because of the small currents (1–10 μA in our experiments) it is not very difficult to produce higher applied fields. To avoid crystal damage in this case the crystal was put into a pressure chamber capable to endure a pressure of up to 10 bar. Our experiments were carried out with a pressure of 3 bar which made it possible to apply an electric field of 10 kV/cm for further increase of contrast. Fig. 7 shows the pressure chamber we used. Operation in a vacuum of less than 10 μbar should be possible too, the technical realization of a pressure of 3 bar seems to be easier.

Figs. 8 and 9 show the difference in modulation caused by different applied electric fields E_0 (see formula (6)).

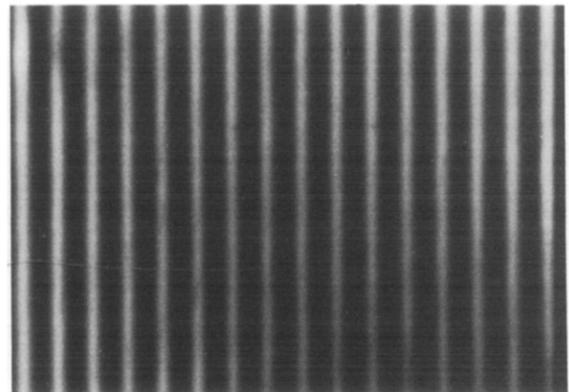


Fig. 8. Stored picture of a lattice. Extant electric field 10 kV/cm.

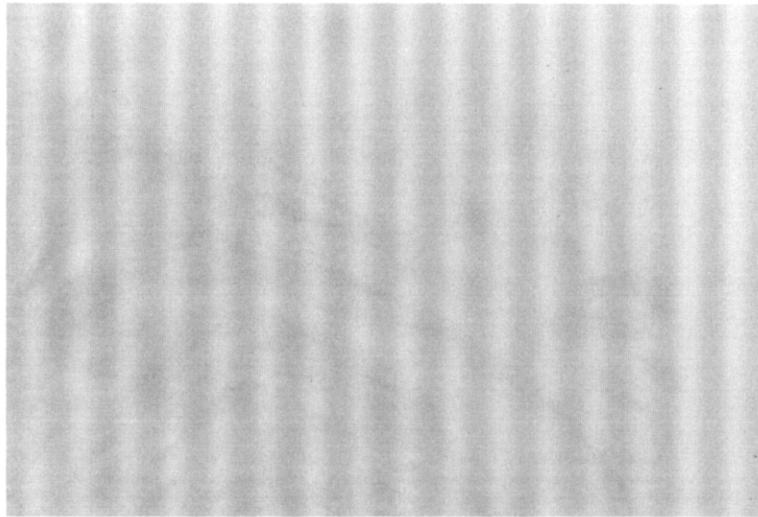


Fig. 9 Stored picture of a lattice. Except for the size of the extant electric field (2 kV/cm instead of 10 kV/cm) all physical conditions are the same as in fig. 8

The response time mainly depends on the illuminance, the applied electric field, and on the wavelength of the light. By illuminating the crystal with an electronic flash we achieved a response time of about 1 ms.

The crystal is sensitive mainly to blue-green light. When using the crystal as an incoherent to coherent converter this is an advantage. The information can be stored by using blue or green light and can be read out with red or infrared light without erasure of the information.

4. Characterization

The new BSO-spatial light modulator is characterized by

- High spatial resolution mainly limited by geometrical optics due to the thickness of the crystal.
- Response time 100–1 ms, depending mainly on the illuminance.
- The application of a pressure chamber allows the use of high electric fields without the risk of damaging the crystal.
- Maximum contrast is limited by the relation between dark- and photocurrent.
- One material, which is as well photoconductive as electrooptic
- Contrast can be easily reversed.

References

- [1] E. Marom and J. Grinberg, *Appl. Optics* 16 (1977) 3086
- [2] W.P. Bleha, L.T. Lipton, E. Wiener-Avneer, J. Grinberg, P.G. Reif, D. Casasent, H.B. Brown and B.V. Markevitch, *Opt. Eng.* 17 (1978) 371.
- [3] P. Auborg, J.P. Hugnard, M. Hareng and R.A. Mullen, *Appl. Optics* 21 (1982) 3706
- [4] C. Warde, A.D. Fisher, D.M. Cocco and M.Y. Burmawi, *Optics Lett.* 3 (1978) 196
- [5] D. Casasent, *Opt. Eng.* 17 (1978) 344.
- [6] D. Casasent, *Opt. Eng.* 17 (1978) 365.
- [7] K. Hess and R. Dandliker, *Deformable surface spatial light modulator*, Contribution to Horizons de l'Optique 85, Besançon.
- [8] Y. Shu, D. Psaltis, A. Marrakchi and A.R. Tanguay, *Appl. Optics* 22 (1983) 3665.
- [9] A. Feldman, W.S. Brower and D. Horowitz, *Appl. Phys. Lett.* 16 (1970) 201.
- [10] J.P. Hugnard and F. Micheron, *Appl. Phys. Lett.* 29 (1976) 591.
- [11] M. Peltier and F. Micheron, *J. Appl. Phys.* 48 (1977) 3863
- [12] W.G. Cady, *Piezoelectricity*, Vol 2 (Dover Publ., New York, 1964)
- [13] J.P. Herriau, J.P. Hugnard and P. Auborg, *Appl. Optics* 17 (1978) 1851.
- [14] H.J. Tiziani, K. Leonhardt and J. Klenk, *Optics Comm.* 34 (1980) 327.
- [15] J.P. Hugnard and B. Ledu, *Optics Lett.* 7 (1982) 310.