

All Electrochemical Synthesis of Performic Acid Starting from CO₂, O₂, and H₂O

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Driven by anthropogenic climate change, innovative approaches to defossilize the chemical industry are required. Herein, the first all-electrochemical feasibility study for the complete electrosynthesis of the strong oxidizer and effective disinfectant performic acid is presented. Its synthesis is achieved solely from CO₂, O₂, and H₂O in a two-step process. Initially, CO₂ is electrochemically reduced to formate employing Bi₂O₃-based gas diffusion electrodes in a phosphate-buffered electrolyte. Thereby, high formate concentration (500.7 ± 0.6 mmol L⁻¹) and high Faradaic efficiency (86.3 ± 0.3%) are achieved at technically relevant current density (150 mA cm⁻²). Subsequently, the formate acts as (storable) feed

electrolyte for the second electrolysis step. Employing carbon-based gas diffusion electrodes, O₂ is reduced to H₂O₂ and performic acid is directly formed in situ. As before, high H₂O₂ concentration (1.27 ± 0.06 mol L⁻¹) and high Faradaic efficiency (85.3 ± 5.4%) are achieved. Furthermore, performic acid concentration suitable for disinfection is obtained (82 ± 11 mmol L⁻¹). In summary, this innovative feasibility study highlights the potential of combining electrochemical CO₂ reduction with H₂O₂ electrosynthesis, which could provide sustainable access to performic acid in the future.

1. Introduction

The pressing need for a transition to renewable energy sources and sustainable feedstocks has led to increased research into alternative chemical production processes. Electrochemical processes, in particular, are emerging as a promising route for achieving this goal, enabling the direct conversion of renewable electricity into value-added chemical products.^[1–4] Such approaches offer not only a reduction in process emissions, but also the potential to integrate decentralized, onsite manufacturing that can complement renewable energy and systems.

One of the most compelling areas of electrochemical synthesis is the reduction of carbon dioxide (CO₂) and its implementation as a renewable feedstock in the chemical industry. Among the various products generated by the electrochemical CO₂ reduction reaction (*eCO₂RR*), formic acid and formate represent attractive intermediates due to their good storage and transport properties, as well as their versatile applications.^[5–9] Thereby, the aqueous *eCO₂RR* can be performed efficiently using gas diffusion electrodes (GDEs), allowing high current densities up to 1.8 A cm⁻²,^[10] Faradaic efficiencies (FE) exceeding 90%,^[11–14] and operational times of 1000 h.^[15]


Beyond its immediate use, formic acid/formate can serve as versatile platform chemical for synthesizing higher-value products combining subsequent chemical and biological processes. Exemplarily, the use as a feedstock in microbial synthesis offers the option to produce more complex and attractive products,^[16–19] which has been demonstrated exemplarily for the synthesis of the biopolymer polyhydroxybutyrate (PHB) without the need for further downstream processing between *eCO₂RR* and the biosynthesis.^[8,9] Another pathway for formic acid/formate is its utilization for the synthesis of the strong oxidizer and disinfectant performic acid (PFA),^[20–23] which is obtained in the equilibrium reaction of formic acid and hydrogen peroxide. PFA is an attractive disinfectant for several sectors such as the food industry, healthcare, and wastewater treatment, as it is already very effective at low concentrations (<20 mg L⁻¹ ≙ 0.32 mmol L⁻¹).^[24–27] It is also environmentally friendly, especially compared to halogen-based disinfectants. Decomposition leads to CO₂, O₂ and H₂O whereas the formation of harmful disinfection byproducts is largely unlikely.^[27–31] The downside of its high reactivity is that it is not stable and safe enough for storage and needs to be produced onsite shortly before use from formic acid and H₂O₂.^[26,31–35]


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The traditional industrial anthraquinone process for H₂O₂ production is energy intensive, generates organic waste, and is associated with significant CO₂ emissions.^[36] Facing these challenges, H₂O₂ syntheses via the two-electron oxygen reduction reaction (eO₂RR) using GDEs has emerged as an alternative approach to the anthraquinone process. Thereby, FE above 90%,^[37–39] current densities up to 0.5 A cm⁻²,^[39] and operational times in range of 200–1000 h^[40–42] have been already reported.

If H₂O₂ is synthesized electrochemically in the presence of carboxylic acids such as formic acid, PFA is generated in situ. Recently, Schneider and Stöckl^[23] published a comprehensive approach to the indirect and on-demand electrosynthesis of various peroxy acids via in situ generated H₂O₂ on GDEs, including PFA. After 24 h of electrosynthesis in a buffered system with 1 wt% H₃PO₄, 1.47 mol L⁻¹ H₂O₂, and 0.24 mol L⁻¹ PFA have been obtained with FEs of 37.5% and 6.1% (combined FE = 43.6%), respectively.

With this study, the first innovative all-electrochemical feasibility study for the complete electrosynthesis of PFA from CO₂, O₂, and H₂O through a two-step process utilizing GDEs is presented (cf. **Figure 1**). In the first step, CO₂ is electrochemically reduced to formate, which then acts as (storable) feed electrolyte in the second step, where O₂ is reduced to H₂O₂ and PFA is formed in situ. The authors thereby continue the findings of their previous study, where it was shown that phosphate ions/phosphoric acid and a buffered electrolyte are beneficial for PFA synthesis,^[23] leading to the initial eCO₂RR in a phosphate-buffered electrolyte solution.

This approach not only highlights the potential of combining CO₂ reduction with H₂O₂ synthesis, but demonstrates the advantages of electrochemical processes like decentralized and on-demand production using the example of PFA, a highly effective oxidant and disinfectant that is not stable and safe enough for storage.

2. Results and Discussion

2.1. GDE Fabrication and Characterization for eCO₂RR and eO₂RR

GDEs for eCO₂RR were fabricated by heat pressing a catalyst mixture onto Ni foam as support material and current collector according to the oxygen-depolarized cathode (ODC) technology developed by Covestro.^[43] The catalyst mixture consisted of Bi₂O₃ nanopowder (≈200 € kg⁻¹) as electrocatalyst and polytetrafluoroethylene (PTFE, ≈50 € kg⁻¹) powder as a hydrophobic binder. Taking contemporary costs into account, the GDE's material cost was estimated at 474 € m⁻², of which Ni foam (≈338 € m⁻²) accounts for 71.3%. In total, three GDEs (*n* = 3) were fabricated for formate feed generation via eCO₂RR. The reproducibility of the predominantly manual fabrication method was sufficient, resulting in GDEs with catalyst loading *b* (Bi₂O₃, wt%) = 65.7 ± 0.7 mg cm⁻² and thickness *d* = 523 ± 11 μm (*n* = 3). Furthermore, no influence of minor fabrication variations on GDE performance was observed.

GDEs for eO₂RR were fabricated in a similar manner as described above, their composition and part of the pressing protocol (excluding sintering at 340 °C) was based on Kopljar et al.^[44] The catalyst mixture consisted of acetylene black powder (≈320 € kg⁻¹) as carbon-based electrocatalyst and PTFE powder as binder. The mixture was pressed onto stainless steel mesh (≈10 € m⁻²) using a cylindrical mask. Afterward, GDEs were treated in a heat press to improve their mechanical stability. In total, eight GDEs (*n* = 8) were fabricated with a catalyst loading of *b* = 26.1 ± 0.5 mg cm⁻² and a thickness of *d* ≈ 600 ± 10 μm. Based on recent prices, the GDE's material cost was estimated at 62 € m⁻².

Both fabricated GDE types were characterized before and after electrolysis by contact angle measurement, density measurement, and scanning electron microscopy (SEM). Exemplary results are summarized in **Figure 2**.

The pristine Bi₂O₃ GDE was bright yellow in color, had a contact angle of 136.2 ± 0.3° (*n* = 2) and a density of 7.060 ± 0.002 g cm⁻³

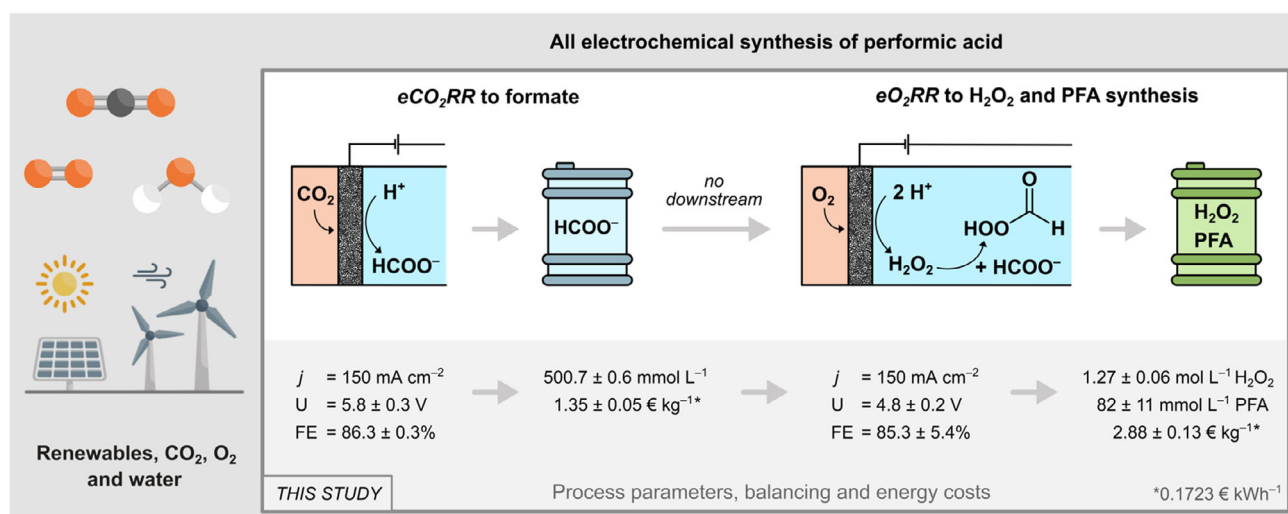


Figure 1. Schematic illustration and key process data of the overall process combination of the electrochemical CO₂ reduction reaction (eCO₂RR) to formate with the electrochemical O₂ reduction reaction (eO₂RR) to H₂O₂ to synthesize PFA using renewable energy sources. Resulting costs for formate and H₂O₂/PFA were based on a recent energy price.^[47] Abbreviations: *j* = current density, *U* = average cell voltage, FE = Faradaic efficiency.

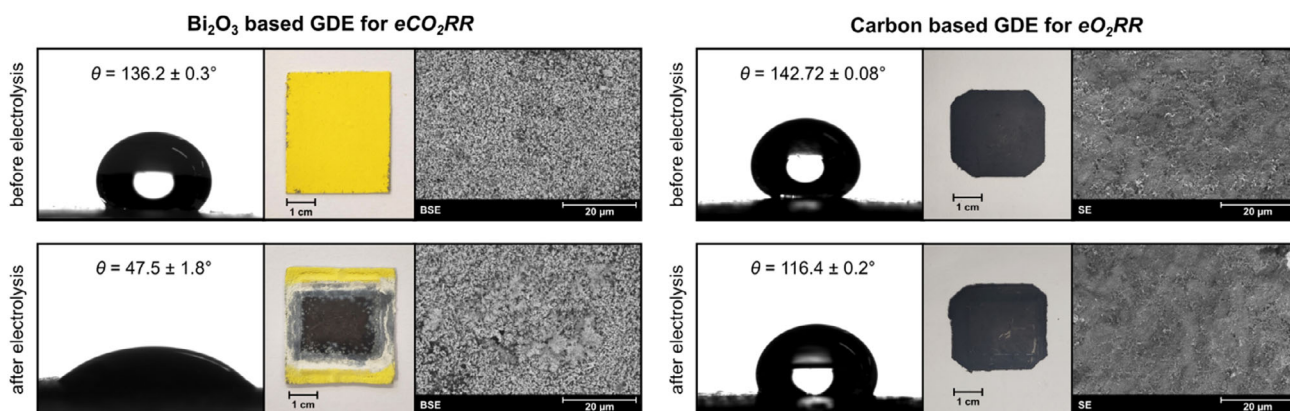


Figure 2. Fabricated GDE for eCO₂RR (left) and eO₂RR (right) and their characterization before and after electrolysis using SEM imaging (BSE = back scattering electrons, SE = secondary electrons) and contact angle measurements.

($n = 3$), and showed evenly distributed, mostly round Bi₂O₃ particles in the SEM (back-scattering electrons) image. After electrolysis, the GDE showed a black discoloration of the area exposed in the flow cell during electrolysis. This was attributed to the reduction of Bi₂O₃ to elemental Bi at the beginning of the electrolysis, which was supported by X-ray diffraction results (cf. Supporting Information). Accordingly, the discolored GDE area had a lower density of $6.631 \pm 0.004 \text{ g cm}^{-3}$ ($n = 3$). The discoloration was further examined using SEM, whereby new dendritic structures were observed. Alongside or in addition to Bi₂O₃ reduction, cathodic corrosion^[45] could have contributed to the change in the GDE's surface structure. Therefore, GDE stability was investigated and will be discussed later regarding feed characterization. Apart from optical changes, the GDE's contact angle decreased significantly to $47.5 \pm 1.8^\circ$ ($n = 2$) after electrolysis. It therefore became relatively hydrophilic during electrolysis, which was expected due to electrowetting.

The carbon GDE for eO₂RR did not show significant optical differences or changes in the GDE surface via SEM either before or after electrolysis. However, the contact angle changed from $142.72 \pm 0.08^\circ$ ($n = 2$) to $116.4 \pm 0.2^\circ$ ($n = 2$) after electrolysis. Consequently, this GDE type was also wetted during electrolysis but remained relatively hydrophobic compared to Bi₂O₃ GDEs. Moreover, the initial GDE density of $3.094 \pm 0.004 \text{ g cm}^{-3}$ ($n = 3$) increased to $3.270 \pm 0.001 \text{ g cm}^{-3}$ ($n = 3$). This density increase might have been caused by salt residues within the GDE, although no significant GDE swelling was observed.

2.2. eCO₂RR to Formate

To generate the formate feed for subsequent H₂O₂ electrosynthesis and PFA generation, eCO₂RR was carried out with Bi₂O₃ GDEs in a gas-fed flow reactor (divided cell, cf. Experimental Section) using $0.2 \text{ mol L}^{-1} \text{ KH}_2\text{PO}_4/\text{K}_2\text{HPO}_4$ (equimolar, pH ≈ 6.67) as both anolyte and catholyte. Phosphate buffer was chosen as a supporting electrolyte based on the results from Schneider and Stöckl^[23] for peroxy acid synthesis using electrochemically generated H₂O₂. Furthermore, promising results were obtained using this electrolyte with Sn-based GDE.^[9] Generally, the aim was to generate a

feed with high formate concentration ($>0.5 \text{ mol L}^{-1}$) at high FE ($>85\%$). For this purpose, all electrolyses were run 22 h at 150 mA cm^{-2} . **Figure 3** contains the courses of formate concentration and FE in the catholyte.

Formate concentration increased linearly over time, its course was fitted in two intervals to obtain the respective formate production rate. It shows the rate declined about 20% from $24.4 \pm 0.2 \text{ mmol L}^{-1} \text{ h}^{-1}$ (interval 1 = 1–5 h, $\pm 113 \pm 1 \text{ mg h}^{-1} \text{ cm}^{-2}$) to $19.5 \pm 0.7 \text{ mmol L}^{-1} \text{ h}^{-1}$ (interval 2 = 20–22 h, $\pm 89.8 \pm 3.2 \text{ mg h}^{-1} \text{ cm}^{-2}$) during runtime. This decline could be attributed to presumed formate mass transport limitations within the GDE's pore system, which would increase the influence of the parasitic hydrogen evolution reaction (HER). Additionally, the decline could also be caused by a possible decrease in the

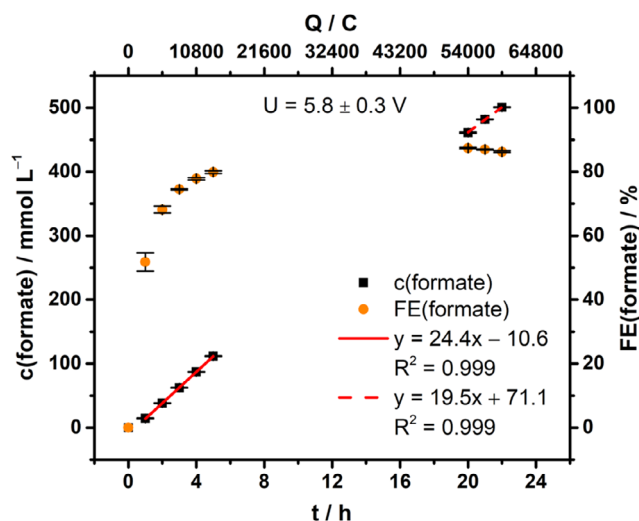


Figure 3. Concentration and FE course of formate for formate electrosynthesis ($n = 3$). The formate concentration course was fitted linearly in two intervals: $t = 1\text{--}5 \text{ h}$ (red, solid line) and $t = 20\text{--}22 \text{ h}$ (red, dashed line). Electrolysis parameters: constant current density $j = 150 \text{ mA cm}^{-2}$, runtime = 22 h ($\pm 59,400 \text{ C}$), electrolyte = $0.2 \text{ mol L}^{-1} \text{ KH}_2\text{PO}_4/\text{K}_2\text{HPO}_4$, initial V (catholyte, anolyte) = 500 mL each, cathode (GDE) = 87.5 wt% Bi₂O₃, 12.5 wt% PTFE on Ni-foam, reference electrode = reversible hydrogen electrode (RHE), anode = mixed Ir-oxide on a Ti-grid (Platinode EP, Type 177, Umicore).

GDE's stability during electrolysis (cf. feed characterization). Nonetheless, a final formate concentration of $500.7 \pm 0.6 \text{ mmol L}^{-1}$ ($n = 3$) was achieved.

Moreover, formate FE shows a nonlinear increase in the first 5 h runtime, especially the FE at 1 h is rather low with $52 \pm 3\%$ ($n = 3$). On the one hand, this is likely caused by partial consumption of supplied charge to reduce Bi_2O_3 to Bi. On the other hand, the GDE's electrowetting behavior could have contributed to the low initial FE. Nonetheless, to reach an overall FE of $79.9 \pm 0.5\%$ ($n = 3$) during the first 5 h, the FE per hour must have been close to 90% after the initial first hour. Consequently, the Bi_2O_3 type GDEs fabricated herein have a peak FE performance of close to 90%. Overall, $86.3 \pm 0.3\%$ ($n = 3$) was achieved as final formate FE in 22 h runtime.

Regarding energy demand, electrolyses were run with an average cell voltage of $5.8 \pm 0.3 \text{ V}$ ($n = 3$). This relatively high cell voltage was mainly caused by ohmic losses in the anode chamber, as a nonzero-gap anode was used for the oxygen evolution reaction (OER) as counter reaction, the GDEs' average potential was only $-1.21 \pm 0.03 \text{ V}$ versus RHE ($n = 3$, cf. Supporting Information). However, the GDEs' potential is also relatively high, possibly due to bismuth's low electric conductivity ($0.936 \times 10^6 \text{ S m}^{-1}$ at 298 K).^[46] In total, electrolyses consumed $96 \pm 4 \text{ Wh}$ ($n = 3$) of electric energy. Hence, formate electrosynthesis required $7.9 \pm 0.3 \text{ kWh kg}^{-1}$, which corresponds to $1.35 \pm 0.05 \text{ € kg}^{-1}$ formate (no downstream processing etc., $0.1723 \text{ € kWh}^{-1}$,^[47] cf. Figure 1). This is higher than market prices for fossil-based concentrated formic acid such as 0.37 and 0.69 € kg^{-1} ($0.40 \text{ \$ kg}^{-1}$ ^[48] and $0.74 \text{ \$ kg}^{-1}$,^[49] respectively with $1 \text{ €} \triangleq 1.08 \text{ \$}$). Consequently, lowering cell voltage and thereby energy demand of $e\text{CO}_2\text{RR}$ are essential to compete with current fossil-based market prices. As discussed above, the integration of a zero-gap anode could lower cell voltage significantly.

2.3. $e\text{O}_2\text{RR}$ to H_2O_2 and PFA Synthesis

In the next step, the generated formate feed ($\text{pH} \approx 4.12$, formic acid $\text{pK}_a = 3.75$ at 25 °C)^[50] was used as catholyte for H_2O_2 electrosynthesis and PFA generation. It was carried out with the same flow cell setup as above, but employing carbon-based GDEs.

All electrolyses were run 6 h at 150 mA cm^{-2} , catholyte samples were taken every 1.5 h to determine H_2O_2 and PFA ($\text{pK}_a = 7.3$ at 25 °C)^[50] concentrations by two-step titration^[51] (H_2O_2 was first quantified by cerimetry and then PFA by iodometry, $n = 3$ for each sample). Direct FE for H_2O_2 and indirect FE for PFA were calculated based on their determined amounts and under the assumption that H_2O_2 and formate react equimolar with each other to form PFA (cf. Equation (2), Experimental Section). A rapid adjustment of the reaction's equilibrium was assumed based on Schneider and Stöckl^[23] results. The combined FE therefore corresponds to the actual FE of H_2O_2 electrosynthesis. Figure 4 summarizes the concentration and corresponding FE courses obtained during electrolysis ($n = 4$).

H_2O_2 concentration increased linearly over time up to $1.27 \pm 0.06 \text{ mol L}^{-1}$ ($n = 4$) in 6 h. After initial GDE conditioning, a production rate of $20.5 \pm 0.9 \text{ mmol L}^{-1} \text{ h}^{-1}$ ($\triangleq 6.97 \pm 0.31 \text{ mg h}^{-1} \text{ cm}^{-2}$)

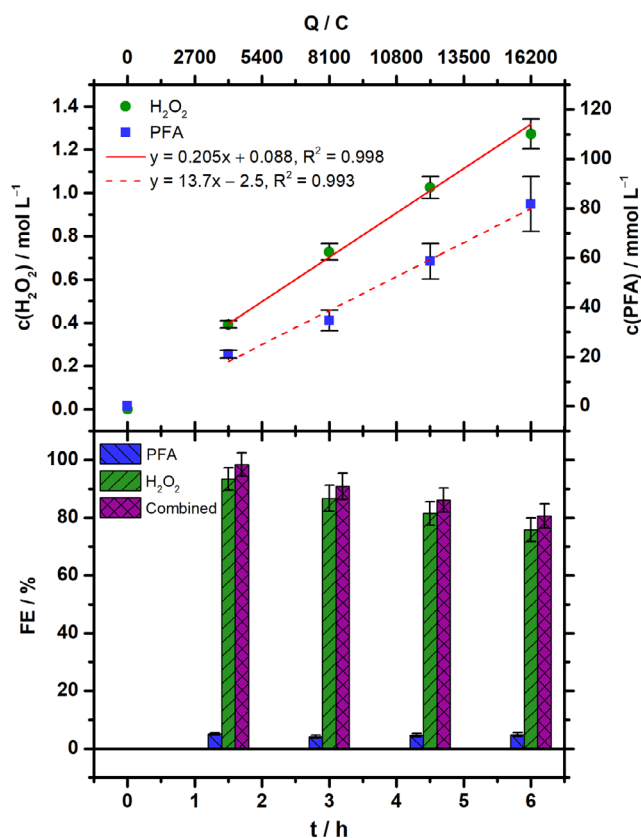


Figure 4. Concentration and FE course of H_2O_2 and PFA for H_2O_2 electrosynthesis and PFA generation ($n = 4$). Electrolysis parameters: constant current density $j = 150 \text{ mA cm}^{-2}$, runtime = 6 h ($\triangleq 16,200 \text{ C}$), catholyte = formate containing catholyte originating from $e\text{CO}_2\text{RR}$ to formate (50 mL), anolyte = $0.5 \text{ mol L}^{-1} \text{ HClO}_4$ (50 mL), cathode (GDE) = 65.5 wt% acetylene black, 34.5 wt% PTFE on stainless steel mesh, reference electrode = reversible hydrogen electrode (RHE), anode = mixed Ir-oxide on a Ti-grid (Platinum EP, Type 177, Umicore).

was reached ($t = 1.5\text{--}6 \text{ h}$). This was accompanied by a continuous increase in PFA concentration ($13.7 \pm 1.2 \text{ mmol L}^{-1} \text{ h}^{-1}$, $t = 1.5\text{--}6 \text{ h}$) to finally $82 \pm 11 \text{ mmol L}^{-1}$ ($n = 4$). Despite the concentration's increase, H_2O_2 FE declined by about 17% from initially $93 \pm 4\%$ ($n = 4$) down to $76 \pm 5\%$ ($n = 4$) during runtime (50 mL catholyte volume assumed). This also applies to the combined FE, so the actual H_2O_2 FE, as the PFA's indirect FE remains nearly constant at 4–5% due to its reaction equilibrium. However, the final H_2O_2 FE had to be corrected to account for an observed increase in catholyte volume after electrolysis. Thereby, a combined H_2O_2 FE of $85.3 \pm 5.4\%$ ($n = 4$) was achieved in 6 h runtime. The FE balance is most likely closed by parasitic HER, but four-electron oxygen reduction to H_2O and/or H_2O_2 decomposition during electrolysis cannot be fully excluded. However, significant decomposition of H_2O_2 /PFA after electrolysis was not indicated (e.g., gas evolution/titration results, cf. Supporting Information).

Electrolyses were run with an average cell voltage of $4.8 \pm 0.2 \text{ V}$ ($n = 4$) consuming $21.5 \pm 0.6 \text{ Wh}$ ($n = 4$) of electric energy. As before, this is a relatively high cell voltage caused by the ohmic losses due to OER at the nonzero-gap anode, the GDEs' potential was only $-1.4 \pm 0.5 \text{ V}$ versus RHE ($n = 4$, cf. Supporting Information). Consequently, H_2O_2 required $8.9 \pm 0.6 \text{ kWh kg}^{-1}$

($n = 4$) corresponding to $1.53 \pm 0.11 \text{ € kg}^{-1}$ as electric energy cost (no downstream processing etc., $0.1723 \text{ € kWh}^{-1}$,^[47] cf. Figure 1). In comparison, fossil-based market prices for concentrated H_2O_2 are in the range of $0.64\text{--}1.1 \text{ € kg}^{-1}$ ($700\text{--}1200 \text{ \$ t}^{-1}$, with $1 \pm 1.08 \text{ \$}$).^[52] For the target byproduct PFA, a yield of $16.3 \pm 2.2\%$ ($n = 4$) was obtained. To achieve higher PFA concentrations/yields, higher concentrations of H_2O_2 and formate are necessary. This is also supported by Greenspan's^[53] results on PFA formation. Taking presumed formate and H_2O_2 energy costs into account, the H_2O_2 /PFA product solution cost added up to $2.88 \pm 0.13 \text{ € kg}^{-1}$ ($n = 4$). As PFA is usually generated onsite of its application, no commercial price was available as reference.

For comparison, H_2O_2 electrosynthesis for PFA generation was also performed with a reference electrolyte (R) based on the formate feed generated via $e\text{CO}_2RR$. It was prepared from commercially available compounds and contained $0.2 \text{ mol L}^{-1} \text{ KH}_2\text{PO}_4/\text{K}_2\text{HPO}_4$ (equimolar) and $0.5 \text{ mol L}^{-1} \text{ HCOOK/HCOOH}$ (equimolar) in $1 \text{ wt\% H}_3\text{PO}_4$. It was adjusted to $\text{pH} = 4.13 \pm 0.05$ with KOH. Using (R) as catholyte, H_2O_2 and PFA showed concentration and FE courses similar to the results presented above, whereas overall values were slightly lower. In short, a combined H_2O_2 FE of $78 \pm 7\%$ ($n = 4$) was obtained in combination with $13.7 \pm 0.8\%$ ($n = 4$) PFA yield. Hence, the formate feed can be generated via $e\text{CO}_2RR$ with slight improvements instead of performance losses for H_2O_2 electrosynthesis and PFA generation. Details are provided (Section S3.2.2, Supporting Information).

So far, only a few results have been published on (indirect) electrochemical PFA synthesis. Recently, Sun et al.^[54] conceptually reported an all-electrochemical PFA synthesis with parallel $e\text{CO}_2RR$ and $e\text{O}_2RR$ using their trifunctional indium-based catalyst/electrolysis system. Furthermore, Kolyagin et al.^[20] used 1.5 mol L^{-1} formic acid ($+0.2 \text{ mol L}^{-1} \text{ K}_2\text{SO}_4$ and $0.05 \text{ mol L}^{-1} \text{ H}_2\text{SO}_4$) as electrolyte solution for $e\text{O}_2RR$ to H_2O_2 with a carbon-based GDE. Thereby, they achieved $1.8 \text{ mol L}^{-1} \text{ H}_2\text{O}_2$ (55% FE) and 6.5 mmol L^{-1} PFA in 7 h electrolysis at 100 mA cm^{-2} .

Schneider and Stöckl^[23] recently published a new benchmark for the indirect electrosynthesis of PFA among various peroxy acids via in situ generated H_2O_2 on commercial carbon black GDEs, as mentioned in the introduction. Thereby, $0.77 \text{ mol L}^{-1} \text{ H}_2\text{O}_2$ (69% FE) and 0.14 mol L^{-1} PFA (13% FE) were achieved in 6 h at 100 mA cm^{-2} with $1 \text{ mol L}^{-1} \text{ HCOOH/HCOOK}$ ($+1 \text{ wt\% H}_3\text{PO}_4$) as electrolyte solution. This corresponded to a combined FE of 82% for H_2O_2 electrosynthesis. Compared to these previous results, H_2O_2 concentration ($1.27 \pm 0.06 \text{ mol L}^{-1}$) and combined FE ($85.3 \pm 5.4\%$) were improved at increased current density (150 mA cm^{-2}) herein. In contrast, PFA concentration ($82 \pm 11 \text{ mmol L}^{-1}$) was lower, which is most probably attributed to the lower initial formate concentration of the formate feed

used as electrolyte solution. Nonetheless, $82 \pm 11 \text{ mmol L}^{-1}$ PFA represents the first benchmark for an all-electrochemical approach to PFA synthesis using CO_2 , O_2 , and H_2O to the best of the authors' knowledge. Even though there is space for improvement in terms of electrolysis and reaction/equilibrium adjustment to reach higher PFA concentrations, the obtained PFA/ H_2O_2 mixture could most likely already be applied for disinfection. On the one hand, far lower PFA concentrations ($<20 \text{ mg L}^{-1} \pm 0.32 \text{ mmol L}^{-1}$)^[24,26,27] have been reported as sufficient for disinfection. On the other hand, a mixture of H_2O_2 , formic acid, and PFA could be advantageous, as synergistic effects have been reported for comparable mixtures.^[55]

2.4. Feed Characterization/GDE Evaluation

After electrolysis, both formate feed and H_2O_2 /PFA product solution were further examined for characterization and to evaluate GDE stability. On the one hand, K^+ and PO_4^{3-} concentrations were determined by ion chromatography (IC) to examine possible differences compared to their initial concentrations. These results were also used to prepare reference electrolyte (R) as formate feed substitute for H_2O_2 electrosynthesis and PFA generation. On the other hand, all solutions were screened via inductively coupled plasma atomic emission spectroscopy (ICP-OES) for metal ions originating from the GDEs as well as other impurities that could decompose H_2O_2 /PFA. Detected target elements were Bi (electrocatalyst $e\text{CO}_2RR$), Ni (support material $e\text{CO}_2RR/e\text{O}_2RR$), Cr and Fe (support material $e\text{O}_2RR$, respectively). Hence, their concentrations were quantified via calibration to investigate cathodic corrosion^[45] and thus GDE stability. The characterization results are summarized in Table 1.

IC analysis revealed the formate feed's PO_4^{3-} concentration was slightly lower (7%) than the initial phosphate buffer, which is due to an increase in volume by osmosis during electrolysis. Moreover, PO_4^{3-} concentration decreases further by about 20% during $e\text{O}_2RR$. This decrease cannot be explained solely by a volume increase or by losses due to a concentration gradient to the anolyte (HClO_4), as the anolyte's phosphate concentrations remained below 0.8 mmol L^{-1} (cf. Section S1.12, Supporting Information).

Besides, K^+ concentration was almost doubled after $e\text{CO}_2RR$. Nearly all K^+ ions are found in the formate feed due to migration, their molar amount in the electrolyte system was constant. In contrast, K^+ concentration was about 22% lower in the H_2O_2 /PFA product solution. Some K^+ was found in the anolyte ($12.6 \pm 1.8 \text{ mmol L}^{-1}$, $n = 3$) but its molar amount was not constant.

Although no GDE swelling was observed, it was presumed both K^+ and PO_4^{3-} discrepancies were caused by salt precipitation

Table 1. Catholyte/feed composition before and after formate as well as H_2O_2 electrosynthesis for PFA generation. K^+ and PO_4^{3-} concentrations were determined via IC and Bi^{3+} , Cr^{3+} , Fe^{3+} , and Ni^{2+} concentrations were quantified via ICP-OES.

	$c(\text{K}^+)$ [mmol L^{-1}]	$c(\text{PO}_4^{3-})$ [mmol L^{-1}]	$c(\text{Bi}^{3+})$ [$\mu\text{mol L}^{-1}$]	$c(\text{Cr}^{3+})$ [$\mu\text{mol L}^{-1}$]	$c(\text{Fe}^{3+})$ [$\mu\text{mol L}^{-1}$]	$c(\text{Ni}^{2+})$ [$\mu\text{mol L}^{-1}$]
$0.2 \text{ mol L}^{-1} \text{ KH}_2\text{PO}_4/\text{K}_2\text{HPO}_4$ ($n = 1$)	286.2	197.5	0	0.270 ± 0.013	2.71 ± 0.05	0.13 ± 0.04
Formate feed ($n = 3$)	542 ± 6	183.4 ± 0.4	0.6 ± 0.4	0.224 ± 0.004	1.67 ± 0.15	0.41 ± 0.17
H_2O_2 /PFA solution ($n = 4$)	423 ± 28	147 ± 10	0.18 ± 0.06	0.23 ± 0.04	1.83 ± 0.14	0.55 ± 0.19

within the carbon-based GDE. This hypothesis is supported by the GDEs' increased density after eO_2RR as discussed previously.

For ICP-OES analysis, the phosphate buffer was examined before characterization of formate feed and product solution. It already contained traces of the identified target elements Cr, Fe, and Ni, which originate from the compounds used for electrolyte preparation. Besides, ICP-OES analysis found only traces of dissolved Bi in the formate feed after eCO_2RR . Its concentration was even lower after eO_2RR due to dilution, as expected for carbon-based GDEs. In general, these traces were above detection but below quantification limit, which resulted in relatively high standard deviations (30–40%). Furthermore, quantification was challenging due to strong matrix effects, as it was observed that Bi^{3+} partly precipitated as $BiPO_4$ in standards containing matrix (cf. Section S1.11, Supporting Information). Consequently, most $BiPO_4$ could have already precipitated during electrolysis, although no precipitates were observed. Therefore, the extent of Bi's cathodic corrosion cannot be fully assessed but is most likely overall very low, as other studies on Bi as electrocatalyst also suggest.^[56] Additionally, the previously discussed possible loss of GDE stability can neither be confirmed nor ruled out as explanation for performance decline during electrolysis. However, as the formate feed's Bi^{3+} concentration was at least below $1 \mu\text{mol L}^{-1}$, a significant influence on H_2O_2 /PFA generation seemed unlikely. Moreover, the feed's Cr^{3+} and Fe^{3+} concentrations were lower compared to their initial ones due to dilution. In contrast, Ni^{2+} concentration was increased by 32% to $0.41 \pm 0.17 \mu\text{mol L}^{-1}$ ($n = 3$). This shows the Bi_2O_3 GDE's support material Ni foam was in contact with catholyte solution and was slightly affected by cathodic corrosion.

Further analysis of the H_2O_2 /PFA solution after eO_2RR revealed Cr^{3+} concentration remained relatively constant, while Fe^{3+} and Ni^{2+} concentrations increased slightly. As the feed is diluted during electrolysis ($\approx 5\%$), molar amounts of all three elements were increased by cathodic corrosion of the stainless steel mesh (1.4301) serving as support material. Nonetheless, all concentrations were rather low and did not seem to have compromised H_2O_2 /PFA generation, especially in the presence of phosphate ions acting as possible chelating agents.^[57]

However, the future aim should be to minimize overall metal ion impurities to avoid potential efficiency losses, as these could potentially catalyze H_2O_2 /PFA decomposition.^[31,58–60]

Furthermore, Schneider and Stöckl^[23] hypothesized that leached Ni may have affected their H_2O_2 electrosynthesis for PFA generation. Although only a total of $0.55 \pm 0.19 \mu\text{mol L}^{-1}$ Ni was leached from the self-fabricated GDEs presented, future GDEs should ideally be realized without metallic support material (without compromising performance and stability).

3. Conclusion

In this study, the first all-electrochemical PFA synthesis has been achieved by coupling eCO_2RR to formate with eO_2RR to H_2O_2 without any intermediate downstream processing.

The formate feed was generated as catholyte by electrochemical CO_2 reduction using Bi_2O_3 GDEs (474 € m^{-2}), which were self-fabricated by a fast, facile, and reproducible fabrication method.

The GDEs were operated at 150 mA cm^{-2} for 22 h to generate a feed containing $500.7 \pm 0.6 \text{ mmol L}^{-1}$ ($n = 3$) formate with a pH of 4.12. Thereby, an overall formate FE of $86.3 \pm 0.3\%$ ($n = 3$) was achieved, while a peak FE up to 90% was reached. Furthermore, no significant cathodic corrosion was observed for the GDEs, Bi^{3+} concentration was at least below $1 \mu\text{mol L}^{-1}$, and Ni^{2+} concentration was below $0.6 \mu\text{mol L}^{-1}$.

The subsequent eO_2RR to H_2O_2 was carried out with the formate feed as catholyte at self-fabricated, inexpensive carbon GDEs (62 € m^{-2}). They were operated at 150 mA cm^{-2} for 6 h without significant cathodic corrosion, whereby $1.27 \pm 0.06 \text{ mol L}^{-1}$ ($n = 4$) H_2O_2 and $82 \pm 11 \text{ mmol L}^{-1}$ ($n = 4$) PFA were reached. This corresponded to an overall H_2O_2 FE of $85.3 \pm 5.4\%$ ($n = 4$) and a PFA yield of $16.3 \pm 2.2\%$ ($n = 4$). The achieved PFA concentration represents the first benchmark for an all-electrochemical PFA synthesis to the best of the authors' knowledge. Furthermore, it already exceeds concentrations suitable for disinfection ($< 20 \text{ mg L}^{-1} \triangleq 0.32 \text{ mmol L}^{-1}$).^[24,26,27]

Finally, electric energy costs of the overall process were assessed for formate ($1.35 \pm 0.05 \text{ € kg}^{-1}$), H_2O_2 ($1.53 \pm 0.11 \text{ € kg}^{-1}$), and H_2O_2 /PFA ($2.88 \pm 0.13 \text{ € kg}^{-1}$) under recent and realistic assumptions ($0.1723 \text{ € kWh}^{-1}$ ^[47]). These costs were ≈ 2 – 3 times higher than fossil-based market prices for formic acid and H_2O_2 , which already include all costs beyond electricity. Consequently, the energy demand for eCO_2RR to formate and eO_2RR to H_2O_2 must be reduced in the future. Nonetheless, this feasibility study demonstrates that an all-electrochemical PFA synthesis from CO_2 , O_2 , and H_2O is a promising approach for new sustainable chemical production processes, which should be investigated further to evaluate potential technical exploitation.

4. Experimental Section

Gas Diffusion Electrodes: Bi_2O_3 -Based GDE

The GDEs were fabricated by pressing the catalyst mixture onto Ni foam as support material. The catalyst mixture (30.00 g) consisted of Bi_2O_3 (87.5 wt%, 26.25 g, purity 99.9%, particle size $\approx 80 \text{ nm}$, US Research Nanomaterials, Houston, USA) and polytetrafluoroethylene (PTFE) powder (12.5 wt%, 3.75 g, Dyneon PTFE TF 2072Z, 3M, Saint Paul, USA). The mixture was homogenized in a knife mill (30 s, 25,000 rpm, 2 \times). Afterward, it (4.00 g) was equally distributed onto Ni foam ($d = 1.4 \text{ cm}$, $3.5 \text{ cm} \times 4.0 \text{ cm} \times 14 \text{ cm}^2$, Ni-5763, density 420–450 g m^{-2} , Recemat BV, Dodewaard, Netherlands) with a sieve and a stencil (cut-out $3.5 \text{ cm} \times 4.0 \text{ cm}$). The GDE blank was placed in between ordinary baking sheet and compressed in a heat press (plate temperature 120 °C, pressure 10 bar, duration 60 s). Excess material was removed, the GDE's catalyst loading b was determined by differential weighing, and its thickness d was measured at the center point.

Gas Diffusion Electrodes: Carbon-Based GDE

The GDEs were fabricated by pressing catalyst mixture consisting of carbon catalyst (65.5 wt%, 1.97 g, acetylene black, 100% compressed, $> 99.9\%$, Alfa Aesar, Haverhill, USA) and PTFE powder (34.5 wt%, 1.03 g, as above) onto a stainless steel mesh (Material 1.4301, mesh size = 0.5 cm, $d = 240 \mu\text{m}$, $3.2 \text{ cm} \times 3.2 \text{ cm}$, Haver & Boecker, Oelde, Germany) as support material. The catalyst mixture was homogenized (as above) and placed (500 mg) in a cylindrical mask ($d = 40 \text{ mm}$) containing stainless steel mesh. The GDE blank was

compressed in a hydraulic press (pressure 3.5 t, 60 s, RT followed by pressure 7 t, 180 s, RT). Afterward, the GDEs were treated in a heat press (plate temperature 120 °C, pressure 10 bar, duration 180 s) to improve their mechanical stability. Catalyst loading b and thickness d of the GDEs were determined as described above.

Gas Diffusion Electrodes: Scanning Electron Microscopy

SEM imaging was performed on Flex SEM 1000 II (Hitachi, Tokyo, Japan) using the following conditions: 15 kV (accelerating voltage), $\times 2000$ (magnification), 6–8 mm (viewing height), 40 (spot size), and SE and BSE (detector). All images were taken at the GDE's geometrical center point.

Gas Diffusion Electrodes: Contact Angles

Contact angles were determined with the OCA 15 plus (DataPhysics Instruments, Filderstadt, Germany). Using the sessile drop method, a droplet of H₂O (50 μ L) was placed at the GDE's center point. Contact angles were calculated by fitting the droplet edges with a Young–Laplace model.

Gas Diffusion Electrodes: Density

GDE densities were determined with the gas pycnometer BELPYCNO L (Microtrac Retsch, Haan, Germany) using helium as probing gas. Samples were measured ($n = 3$) at 20 °C in sample chamber S (20 cm³) using glass beads as filler volume ($\approx 50\%$).

Formate Electrosynthesis

The same electrochemical flow reactor (divided cell with a cation exchange membrane) and electrolysis setup as described in Dinges et al.^[9] were used for formate electrosynthesis.

All formate electrosyntheses were performed for 22 h at 150 mA cm⁻² (750 mA in total) using a power supply unit (NGP804, Rohde & Schwarz, Munich, Germany), which recorded cell voltage, current, and power. The GDE's electrode potential was referenced to RHE without compensation for iR losses.

CO₂ (N4.5) was supplied to the GDE at a flow rate of 10–15 mL min⁻¹ and an initial overpressure in the range of 110–150 mbar relative to ambient pressure.

The buffer 0.2 mol L⁻¹ KH₂PO₄/K₂HPO₄ (equimolar) served as electrolyte, both anolyte and catholyte had a starting volume of 500 mL (volumetric flask, ISO 1042). They were circulated continuously at a flow rate of ≈ 40 mL min⁻¹ between the flow reactor and reservoir, respectively. During electrolysis, catholyte samples (1 mL) were taken hourly in the first five ($t = 0$ –5 h) and the last three ($t = 20$ –22 h) hours to monitor formate concentration and calculate the corresponding FE. After electrolysis, the catholyte volume was determined by its weight and density ($n = 3$). Catholyte-containing formate was stored at 5 °C until its application for H₂O₂ electrosynthesis and PFA generation. The GDE was rinsed with H₂O and dried at RT. Further details are provided (Section S1.4, Supporting Information).

Formate Quantification by High-Performance Liquid Chromatography

Formate concentrations were determined via HPLC (LC-20AD, SIL-20AC HT, CBM-20A, CTO-20AC, SPD-M20A - Shimadzu, Kyoto, Japan).

The HPLC unit was equipped with a Rezex ROA-Organic Acid (8%) column (300 mm \times 7.8 mm, Phenomenex, Torrance, USA) and the

following method parameters were employed: 5 mmol L⁻¹ H₂SO₄, 0.6 mL min⁻¹, 30 °C, 30 \pm 1 bar, photodiode array detector ($\lambda = 194$ nm), 14.9 min (retention time), 25 min (duration).

Formate standards were prepared by a dilution series from a stock solution, which was prepared with HCOONa (3.482 g, 51.2 mmol) in a volumetric flask (100 mL, ISO 1042). All formate standards (8, 16, 32, 64, 128, 256, 512 mmol L⁻¹) were measured ($n = 3$) and their signal areas fitted linearly ($R^2 = 0.9999$, fit forced through zero).

H₂O₂ Electrosynthesis for PFA Generation

The same flow reactor and electrolysis setup were used for H₂O₂ electrosynthesis as for formate electrosynthesis.

All electrolyses were performed for 6 h at 150 mA cm⁻² (750 mA in total) using a power supply unit (HMC8043, Rohde & Schwarz, Munich, Germany), which recorded cell voltage and current. The GDE's electrode potential was referenced to RHE, without compensation of iR losses.

O₂ (N4.6) was supplied to the GDE with a flow rate of 20 mL min⁻¹ and an initial overpressure of ≈ 90 mbar relative to ambient pressure.

Catholyte (Formate feed) and anolyte (0.5 mol L⁻¹ HClO₄) had a starting volume of 50 mL each (measuring cylinder, 100 mL, ISO 4788) and were continuously circulated at a flow rate of ≈ 40 mL min⁻¹ between the flow reactor and the reservoir. HClO₄ was selected as an anolyte to ensure sufficient proton supply to the catholyte. During electrolysis, electrolytes were sampled (1 mL) every 1.5 h to determine H₂O₂/PFA concentrations and calculate their corresponding FE. The catholyte's volume was determined after electrolysis in the same manner as described above. Further details are provided (Section S1.5, Supporting Information).

H₂O₂/PFA Quantification by Titration

The concentrations of H₂O₂ and PFA were determined using a two-step titration method derived from the procedure described by Greenspan and Mackellar.^[51] First, the concentration of H₂O₂ was determined by cerimetry using Ce(SO₄)₂ ($c = 0.01$ mol L⁻¹). For this purpose, 5 drops of H₂SO₄ ($c = 5$ mol L⁻¹) and 70 μ L ferroin ($c = 0.025$ mol L⁻¹ in ethanol) as an indicator were added to the sample solution. The orange solution was titrated until a light blue color was observed. The concentration of PFA was then determined via iodometry with Na₂S₂O₃ ($c = 0.01$ mol L⁻¹). To the light blue solution, 0.1 mL of a KI solution ($c = 0.48$ mol L⁻¹) and a spatula tip of (NH₄)₆Mo₇O₂₄·4H₂O were added. After 15 min, the resulting reddish-brown suspension was slowly titrated until the color changed to light brown. Then 2–3 drops of starch solution (1 wt% v⁻¹) were added and titration continued until the color changed back to orange and no precipitate remained. The sample volumes were 0.2 mL (after 1.5 h), 0.1 mL (after 3.0 h), and 0.075 mL (after 4.5 and 6.0 h). Each titration was carried out in triplicates ($n = 3$) for the specified time and experiment.

Catholyte/Feed Characterization: Ion Chromatography

IC measurements to determine K⁺ concentrations were performed on Dionex ICS-5000⁺ DC (Pre column = Dionex IonPac CG17, Column = Dionex IonPac CS17, Analytical 2 \times 250 mm, Suppressor = CERS 500, 2 mm, Thermo Fisher Scientific, Waltham, USA). Methanesulfonic acid (MSA) served as eluent with a gradient method (steps 1–4: 1. –5–0 min, 1.5 mmol L⁻¹ MSA (preparation step); 2. 0–25 min, 1.5–2.1 mmol L⁻¹ MSA; 3. 25–40 min, 6 mmol L⁻¹ MSA; 4. 40–60 min, 1.5 mmol L⁻¹ MSA) at 0.1 mL min⁻¹ flow rate. Samples were diluted by factor 500 and K⁺ (retention time = 34.9 min) was detected with a conductivity cell.

Standards were prepared by a dilution series of a stock solution. The stock solution was prepared with KCl (1.221 g \pm 640 mg K⁺) in a volumetric flask (1 L, ISO 1042). All standards (2, 4, 8, 16, 32, 64 ppm) were measured ($n=3$) and their signal areas fitted linearly ($R^2 = 0.999$, fit forced through zero).

IC measurements to determine PO₄³⁻ concentrations were performed on Dionex Aquion system (Pre column = Dionex IonPac AS22, 4 \times 50 mm, Column = Dionex IonPac AS22, 4 \times 250 mm, Suppressor = ACRS 500 Suppressor, 4 mm).

The following isocratic method was used: 4.5 mmol L⁻¹ Na₂CO₃/1.4 mmol L⁻¹ NaHCO₃ (eluent), 1.2 mL min⁻¹ (flow rate), 250 μ L (injection volume), 15 min (duration), 9.3 min (retention time), conductivity cell (detector). Samples were diluted by factor 250.

PO₄³⁻ standards were prepared by a dilution series from a stock solution, which was prepared from an anion multielement standard (10 mL, Certipur, Anion multielement standard I, 1000 ppm F⁻, PO₄³⁻, Br⁻, Merck, HC17168637) in a volumetric flask (50 mL, ISO 1042).

All PO₄³⁻ standards (25, 50, 100 mg L⁻¹) were measured ($n = 1$) and their signal areas fitted linearly ($R^2 = 0.999$, fit forced through zero).

Catholyte/Feed Characterization: Inductively Coupled Plasma Optical Emission Spectroscopy

ICP-OES measurements were performed in axial viewing mode on Agilent 5800 ICP-OES equipped with an SPS 4 Autosampler, a borosilicate double-pass spray chamber, and a Seaspray concentric glass nebulizer (Agilent Technologies, Santa Clara, USA).

All catholyte samples were measured without dilution except for acidification to 2 wt% HNO₃ (using 69 wt% HNO₃).

Standards to determine the concentrations of Bi³⁺ ($\lambda = 223.061$ nm), Cr³⁺ ($\lambda = 205.560$ nm), Fe³⁺ ($\lambda = 238.204$ nm), and Ni²⁺ ($\lambda = 231.604$ nm) were prepared by a dilution series of a stock solution (16 mg L⁻¹). The stock solution was prepared by combining the respective standards (10 mL each, 1000 mg L⁻¹, Single Element ICP-Standard-Solution, Carl Roth) in a volumetric flask (100 mL, ISO 1042) using 2 wt% HNO₃ for dilution. Afterward, the solution was diluted further with 2 wt% HNO₃ to 16 mg L⁻¹ in a volumetric flask (50 mL, ISO 1042). This was followed by a dilution series by factor 2. Finally, each standard (0.125, 0.25, 0.5, 1, 2, 4, 8, 16 mg L⁻¹) was diluted again by factor 2 with a matrix solution (0.4 mol L⁻¹ KH₂PO₄/K₂HPO₄, 0.5 mol L⁻¹ HCOOH, 0.5 mol L⁻¹ HCOOK in 2 wt% HNO₃). Thereby, a set of standards with a matrix based on the catholyte's composition was obtained. They were measured ($n = 5$) and their signal areas fitted linearly ($R^2 \geq 0.997$, fit forced through zero). Further details are provided (Section S1.11, Supporting Information).

Calculations

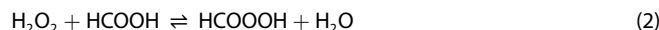
The FE for formate and H₂O₂ were calculated based on the determined amount of electrosynthesized components using Equation (1).

$$FE = \frac{F \cdot z \cdot n}{I \cdot t} \times 100\% \quad (1)$$

with FE = Faradaic efficiency, %; F = Faraday constant, A s mol⁻¹; z = number of transferred electrons ($z = 2$); n = amount of synthesized formate or H₂O₂, mol; I = current, A; t = electrolysis runtime, s.

The results for the different catholytes were averaged and their standard deviation was provided as uncertainty.

The indirect FE for PFA was determined under the assumption formic acid reacted equimolar in a chemical reaction with the electrochemically generated H₂O₂ to PFA using Equation (2).



The combined concentrations and FE of H₂O₂ and PFA were calculated by the addition of the individual mean values. The errors were determined using their standard deviations and Gaussian error propagation using Equation (3).

$$\sigma_{\text{combined}} = \sqrt{\sigma_{\text{H}_2\text{O}_2}^2 + \sigma_{\text{PFA}}^2} \quad (3)$$

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Conflict of Interest

The authors declare no conflict of interest.

Data Availability Statement

Data available in article supplementary material.

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